



DEVELOPMENT PERMIT

NO. **DP- 2018-21**

TO: **Braun Geotechnical**

ADDRESS: **102 19049 95A Street
Surrey, BC V4N 4P3
(Permittee)**

- 1) This Development Permit is issued subject to compliance with all of the Bylaws of the Town of Gibsons applicable thereto, except those specifically varied or supplemented by this Permit.
- 2) The Development Permit applies to those "lands" within the Town of Gibsons described below:

Parcel Identifier: 011-961-929

Legal Description: Reference Plan 18037, LMP21605, District Lot 1328

Civic Address: 464 Eaglecrest Drive

- 3) These lands are within Development Permit Area('s) of the Town of Gibsons Official Community Plan (Bylaw 985, 2005). This permit applies to the following Development Permit Area:
 - Development Permit Area No. 9 (Gibsons Aquifer) for the purpose of the protection of the Gibsons Aquifer.
- 4) The "land" described herein shall be developed strictly in accordance with the terms and conditions and provisions of this Permit, and any plans and specifications attached to this Permit which shall form a part thereof; specifically:
 - Proposed Drilling Program for Proposed Development at 464 Eaglecrest Drive, Braun Geotechnical, September 10, 2018, and letter dated October 24, 2018.
- 5) A minimum of 48 hours notice prior to commencing excavation is to be provided to the Director of Infrastructure Services.
- 6) All requirements of the program are to be followed. On site monitoring by the Braun Geotechnical during pond excavation is required.
- 7) Should the glacial till layer be encountered Braun Geotechnical is to contact the Director of Infrastructure Services prior to continuing excavation.

- 8) Minor changes to the aforesaid program that do not affect the intent of this Development Permit are permitted only with the approval of the Town of Gibsons and Braun Geotechnical.
- 9) If the Permittee does not commence the development permitted by this Permit within twenty four months of the date of this Permit, this Permit shall lapse.
- 10) This Permit is NOT a Building Permit.

ISSUED THIS 1 DAY OF November, 2018.



Lesley-Ann Staats, MCIP, RPP
Director of Planning

Copy of permit to 464 Eaglecrest Drive Properties Ltd., Inc. No. BC1089556

**Proposed Drilling Program
for Proposed Development at
464 Eaglecrest Drive, Gibsons,
BC**

Submitted to: The Town of Gibsons

Date Issued: Sept 10, 2018

PREPARED BY: Braun Geotechnical

CC: Town of Gibsons representative _Dave Newman_____
Town's hydrogeology consultant _Active Earth Engineering_____
Drilling contractor _On Track Drilling Inc_____
Barge Contractor (if applicable) _N/A_____
Other personal on site (if applicable) _N/A_____

CONTACT LIST

EMERGENCY NUMBERS

Town of Gibsons Representative: *Dave Newman, 604 886 2274, 604 741 8370*
Drilling Contractor Owner/Principal: *Joe McKenzie, 778 231 8952*
Ambulance/Hospital **911**

Prime Consultant in Charge

Principal Consultant: *Stuart Hrysio (Braun Geotechnical), ph: 6045134190, cell: 778 238 4712*
Field Consultant: *Hugh MacMurray (Braun Geotechnical), ph: 6045134190, cell: 604 338 7284*

Town Hydrogeology Consultant

Principal Hydrogeologist: *David Kneale, 604-856-5119, 604-312-3891 (c)*
Field Hydrogeologist: *David Kneale, 604-856-5119, 604-312-3891 (c)*

SERVICE COMPANIES

Drilling Contractors: *On Track Drilling Inc, ph: 604 523 1200, cell: 778 231 8952 (Joe)*
Grouting/Cement Contractor: *On Track Drilling (as above)*
Vacuum Truck: *N/A*
Waste Removal Contractor: *N/A*
Barge Operator: *N/A*
Other: *N/A*

TO BE POSTED ON SITE

1 OVERVIEW

1.1 The purpose of subject the drilling program is to:

- Complete 4 x Test Holes drilled with Sonic drill rig to target depth of 7.6 to 12.2m (25 to 40 feet).

As outlined in the Town of Gibsons Development Permit Area Guidelines, the proposed drilling area is underlain by a known artesian aquifer (the Gibson Aquifer) and therefore an increased standard of care is needed to protect the aquifer.

The site is located within the mapped 'Lower Gibsons' aquifer area to the east of Eaglecrest Drive.

Active Earth Engineering (hydrogeologist consultant) consider that the proposed drilling and test pitting program (maximum 12.2m (40ft) drilling depth) will likely penetrate shallow unconfined aquifers with low water production capability but will not reach the confined Gibsons Aquifer. As such surface casing is not required.

Braun Geotechnical envisage that the following risks would be involved in the proposed drilling program:

- Uncontrolled artesian flow if aquitard confining Gibson Aquifer is breached.
- Possible development of a sink hole if artesian flow is left unattended or site workers are unprepared to mitigate the flow.
- Possible impact on the Town of Gibsons' water wells if the aquifer is breached and left unsealed.
- Potential loss of aquifer pressure if the aquifer is breached and not sealed properly.

1.2 Table 1 summarizes the proposed drilling program with anticipated depth, location, and decommissioning plan. The proposed borehole locations are shown on the attached site plan.

Table 1: Example table of proposed borehole details

<i>Borehole Name</i>	<i>Location</i>	<i>Planned Depth (m)</i>	<i>Decommission Plan</i>
<i>TH18-01</i>	<i>As shown on attached location plan</i>	<i>7.6</i>	<i>Backfill with cement based grout (with 5% bentonite)</i>
<i>TH18-02</i>		<i>7.6</i>	
<i>TH18-03</i>		<i>12.2</i>	
<i>TH18-04</i>		<i>12.2</i>	

2 PRE-DRILLING REQUIREMENTS

2.1 The following must be established prior to drilling commencement:

- Knowledge and understanding of British Columbia's Groundwater Protection Regulation
 - (http://www.bclaws.ca/Recon/document/ID/freeside/11_299_2004)
- WorkSafe BC program
 - Avoid drilling where remnant service lines may exist between Eaglecrest Drive and demolished house & shed.
 - Awareness of trip hazards and rough ground, particularly on lower slopes of site.
 - All personnel to wear personal protective equipment including steel cap boots, high viz clothing, eyewear and hearing protection.

Permit Requirements:

Driller certification:

- On Track driller certification provided in appendix under Drilling Contractor Materials.

All rig lifting equipment, and overhead equipment must be certified to the Original Equipment Manufacturers Specifications (OEM).

- The sonic drill was bought new in Jan 2018 , all equipment is original from manufacturer

Casing handling and running procedures:

- The casing and drill pipe will be transported to the drill site via tractor trailer. Once pipe is on site it will be removed from the trailer deck with a skid steer equipped with lifting forks and placed in front of the drill in a pipe rack.
- Two crew members will lift individual pipe onto a hydraulic "pipe handler"
- The "pipe handler" lifts the pipe up into the drill head.

Attachments:

- Certificate of Insurance
- WorkSafe BC letter
- Drill rig specifications

Additional pre-drilling requirements:

- Refer to BC MoE Flowing Artesian Wells document in appendix.

3 RIG MOVE, RIG UP AND SITE SAFETY

3.1 The following procedures/site safety provisions must be followed in mobilizing, set up and operation of the drilling rig:

- *Drilling contractor to contact prime consultant in advance the day before mobilization to site to confirm drill is ready.*
- *Move in and set up drilling rig and auxiliary equipment on site. Prior to initiating drilling, carry out detailed rig inspection and report any unsafe conditions to prime consultant.*
- *Hold a pre-drilling safety meeting with the rig crew and all consultants on site to discuss the Hazardous Operations and drilling program.*
- *Certified driller to be onsite at all times during drilling.*

4 GENERAL DRILLING PROCEDURES

4.1 Roles and responsibilities:

- Prime field consultant and Town's hydrogeology consultant to be onsite to observe soil samples and water conditions within test boreholes.
- Drilling contractor to drill to target depth, collect core samples and measure for water depth once test boreholes are completed.

4.2 Methodology of data and sample collection:

- Formation samples will be continuously retrieved from sonic drilling casing from surface to target depths of test boreholes.

4.3 Drilling Details

4.3.1 Test Holes TH18-01 through TH18-04

- Test Holes will be drilled vertically to approximately 7.6 to 12.2m and logged by the prime field consultant. The actual total depth of test hole will be finalized in the field based on subsurface conditions and soil samples.
- Drilling rate should be sufficiently slow to allow for the collection of core samples by prime field consultant.
- Prime field consultant to complete geological logging, various geotechnical measurements
- Town's hydrogeology consultant to observe process and assist wherever possible.

If the aquifer soil (which is understood to comprise coarse grained sand and/or gravel) and/or artesian pressures or fresh water are encountered, borehole to be abandoned immediately as described below.

- Discontinue drilling with core barrel and place surface casing down to the level where flowing conditions were encountered. Continue drilling with core barrel.
- Refer to BC MoE Flowing Artesian Wells document for guidance.
- Must provide details describing control

4.3.2 Borehole Abandonment Program (Artesian Flowing Well Bore)

- Discontinue drilling with core barrel and place surface casing down to the level where flowing conditions were encountered. Continue drilling with core barrel.
- Measure hydraulic head and contact Active Earth to determine the grout weight required to withstand the hydraulic pressure.
- 5% bentonite to be used in grout mixture.
- Grout to be poured with tremie.
- Confirm that cement/grout has set and sealed before moving off of location.

4.3.3 Borehole Abandonment Program (Non-artesian Flowing Well Bore)

- Discontinue drilling with core barrel and place surface casing down to the level where flowing conditions were encountered. Continue drilling with core barrel.
- 5% bentonite to be used in grout mixture.
- Barite to be used in grout mixture, such that minimum grout weight of 12 lbs/gal is achieved.
- Grout to be poured with tremie.
- Confirm that cement/grout has set and sealed before moving off of location.

5 FIELD PACKAGE

The following documents are attached:

- Proposed borehole location plan
- Active Earth Hydrogeology report
- Site specific Health and Safety Plan
- Drilling Contractor Materials (driller certification, procedures, rig equipment and operation, Insurance, BC Worksafe letter)
- Utility plans
- BC MoE Flowing Artesian Well Document

6 JUNE 2018

DRILLING CONTRACTOR MATERIALS

Driller Certification

Billy Fitzgerald:

- B.C. certified Licenced Well Driller
- Level# 1 first aid, WHIMS,TDG,LPS,POST
- Class3 with air
- Fire extinguisher training
- Hearing test, repertory fit test
- Supervising ground disturbance
- Kinder morgan safety orientation
- BCCSA
- Canadian national safety
- Bear awareness
- Hazard assessment
- 18 years Sonic drill operator

Tim Gilbert:

- Class1 drivers
- H2S alive, H2S aware. POST,TDG, WHIMis
- Cn contractor safety
- Level a first aid
- 6 years sonic drilling experience



**MS-75 TRACK MOUNTED
SONIC DRILL**
GEOTECHNICAL – AUGER & SONIC

MULTIPOWER



FEATURES

Compact & Low impact - Small Footprint & Rubber Track Undercarriage

Powerful - 160 HP Cummins Power Unit

Safe – Rod handler & Guarding

Fast & Efficient – Sonic Drilling Technology Provides a Fast, Accurate Sample



Multi-Sonic MS-75 Track Mounted Sonic Drill

Geotechnical - Auger & Sonic

SPECIFICATIONS

DEPTH CAPACITIES*:	
4.75" (121 mm)	255 ft / 78 m
6" (152 mm)	200 ft / 61 m
7" (178 mm)	170 ft / 52 m
8" (203 mm)	150 ft / 45 m
	*Depending on ground conditions
PRIME MOVER	
Model:	Cummins QSB4.5, 4 cylinder, turbo charged diesel engine
Power:	160 HP @ 2200 RPM
ROTATION UNIT / OSCILLATOR	
Model:	MiniSonic
Frequency range:	0-75 Hz
Output force @ 75 Hz:	41,000 lbs.
Max torque:	1700 ft-lbs.
Rotation speed:	0-80 RPM
TRACK PACKAGE	
Model:	Morooka MST-800 rubber tracked undercarriage
Design:	Hyd. driven piston motors, spring brake, Brevini final drive
Speed:	3 km/h
Max grade:	86% / 39 degree
Control:	Radio remote w/ manual control on rig
BREAK-OUT CLAMP	
Style:	Two hydraulic clamp "double break-out" system
Max opening:	12"
Clamping force:	30,000 lbs.
Breaking torque:	25,000 ft-lbs.
MAST AND FEED	
Design::	Chain over cylinder feed
Pullback:	15,000 lbs.
Pulldown:	10,600 lbs.
Feed stroke:	14 ft.
Working angle:	45 to 90 degree
Rod pull:	10 ft / 3 m lengths
Tilting head:	30 degree side tilt
Mast dump:	48" travel
ROD HANDLER	
Style:	Front mounted, two clamp system
Max clamping diameter:	12"
Rod length:	10 ft / 3 m

HYDRAULIC SYSTEM	
Design:	Fully hydraulic, no electronics, open and closed loop
System pressure:	4500 PSI
Filtration:	10 micron
Heat exchanger:	Air:oil
COOLING	
Ambient temperature rating:	50 Deg C (122 Deg F)
Coolers:	Hydraulic driven fan
CONTROL PANEL	
Engine control:	Complete engine control - ignition, throttle, tach, safety shut-downs
Drill control:	Control handles for all drilling functions
Water control:	Water "tree" w/ gauge and shut-offs
E-stops:	(2) E-stop included
Drive control:	Control valves for manual LH & RH track control
WINCH	
Design:	TH1 planetary style w/ fail safe brake
Pull:	2200 lbs.
Capacity:	100 ft x 1/4" cable
WATER PUMP	
Model:	W1122BCD (435) Piston pump
Max flow:	37 GPM
Max pressure:	1000 PSI
DRILL DECK	
Stabilizers:	(4) Hydraulic stabilizers
Fuel tank capacity:	50 gallon
Storage:	Multiple tool boxes
AUTO HAMMER (OPTIONAL)	
Hammer weight:	140 lbs.
Complete assy. Weight:	323 lbs.
Hammer travel distance:	30"
Percussion rate:	0-50 blows per minute
Mounting arm:	Hydraulic swing in / out
GROUT PUMP (OPTIONAL)	
Model:	Continental 3CL4 progressive cavity pump
Max flow:	14 GPM
Max pressure:	225 PSI
WEIGHT	
27,000 LBS.	



Diamond Core



Seismic



Air Rotary



**Specialty &
Multi-Purpose**

MULTI POWER PRODUCTS LTD

975 CROWLEY AVENUE
KELOWNA BC CANADA
V1Y 9R6

P 250.860.6969
F 250.860.3340

MULTIPOWERPRODUCTS.COM

MULTI▶POWER

MULTIPOWERPRODUCTS.COM

CERTIFICATE OF INSURANCE

This is to certify to: NSCP Design Build LP
100 Bridge Rd, West Vancouver, BC

that policies of insurance as herein described have been issued to the Insured named below and are in force at this date.

NAMED INSURED: Joe Mackenzie O/A On Track Drilling Inc.
On Track Drilling Inc.

MAILING ADDRESS: 107-20626 Mufford Crescent, Langley, BC, V2Y 1N8

OPERATIONS / LOCATION TO WHICH THIS CERTIFICATE APPLIES:

All operations of the Named Insured

Pollution Liability Policy # B088861052H17011 - Effective Feb 2/18 to Feb 2/19

Company Special Risk - \$2,000,000 Pollution Liability

COVERAGE

Commercial General Liability (CGL) - Including:
3rd Party Bodily Injury/Property Damage/Personal Injury

POLICY NO.
501534940

LIMITS OF LIABILITY
\$5,000,000 per occurrence

INSURER(S):

Intact - Acquisition

100%

CGL

EFFECTIVE DATE: 12Jun2018

EXPIRY DATE: 26Jun2019

SPECIAL CONDITIONS & CLAUSES

This certificate is issued as a matter of information only and confers no rights upon the Certificate Holder other than those provided by these policies. The certificate does not amend, extend or alter the coverage afforded by these policies.

The insurance afforded is subject to the terms, conditions and exclusions of the applicable policy.

E&OE



DATE: 12Jul2018

Authorized Representative

THIS POLICY(S) CONTAINS A CLAUSE OR CLAUSES WHICH MAY LIMIT THE AMOUNT PAYABLE

Confirmation of Vehicle Insurance Coverage



Insurance Corporation
of British Columbia
(the Corporation)

NAME OF INSURED (surname followed by given name(s)) ON TRACK DRILLING INC.		
ADDRESS OF INSURED 20626 MUFFORD CRESCENT		
CITY LANGLEY	PROVINCE BC	POSTAL CODE V2Y 1N8

This is to confirm to:

that the following coverage in accordance with the Insurance (Vehicle) Act (the Act), the Insurance (Vehicle) Regulation (the Regulation), and, where applicable, the ICBC Autoplan Optional Policy, is provided to the insured named above and is in force at this date.

This confirmation is issued as a matter of information only and confers no rights on the confirmee and imposes no obligations on the Corporation, or the undersigned representative.

COVERAGE	LICENCE PLATE NO.	LIMIT OF LIABILITY	DESCRIPTION OF VEHICLE			
			YEAR	MAKE	MODEL	VEHICLE IDENTIFICATION NUMBER (VIN)
THIRD PARTY LIABILITY (REGULATION, PART 6) (OPTIONAL POLICY, DIVISION 4)	1. CR3062	\$ 5,000,000.00	1992	INTERNATNA		1HTSDNURXNH419102
	2. CR3064	\$ 5,000,000.00	2018	FORD	F150	1FTEW1EG6JFB14079
	3. 32625U	\$ 5,000,000.00	2013	CAMSUPERLI		5JPBU3629DP031970
	4. 45073U	\$ 5,000,000.00	2016	NOVAE		5JW1U1624G1124018
	5. EL7427	\$ 5,000,000.00	2000	FREIGHTLIN		1FV3GFAC3YHB79210
	6. CR3063	\$ 5,000,000.00	1995	INTERNATNA		1HTSHAAT0SH630611
	7. KS8959	\$ 10,000,000.00	1999	INTERNATNA		1HSHCAHR7XH603677
	8. HV0004	\$ 5,000,000.00	2007	HINO		5PVNE8JL472S50029
	9. LW0317	\$ 5,000,000.00	2014	FORD		1FD0W5HTXEEB83360
	10. MP2876	\$ 5,000,000.00	2007	FREIGHTLIN		1FVHC5DE27HX52411
	11. 28696D	\$ 5,000,000.00	2003	SULAIR		004132531
	12. UNK39C	\$ 5,000,000.00	2003	R-W MFG		09120300010309158
	13.	\$				

AGENT'S COMMENTS PLEASE SEE ATTACHED LIST OF VEHICLES	AGENCY NUMBER 55255
---	-------------------------------

The Motor Vehicle Liability Insurance Card Canada Inter-Province on the back of this Confirmation of Vehicle Insurance Coverage is not valid and does not serve as proof of liability insurance for any vehicle.

Coverage effective from:	Coverage to expire on:
DATE (ddmmyyyy) 01 - 01 - 2018	DATE (ddmmyyyy) 30 - 06 - 2019

SIGNATURE OF AGENT

DATE

NOT VALID UNLESS STAMPED BY AUTHORIZED ISSUING OFFICE
55255
JUL 12 2018



WORKING TO MAKE A DIFFERENCE

Assessment Department

Mailing Address

PO Box 5350
Station Terminal
Vancouver BC V6B 5L5

Location

6951 Westminster Highway
Richmond BC
V7C 1C6
www.worksafebc.com

Clearance Section

Telephone 604 244 6380
Toll Free within Canada
1 888 922 2768
Fax 604 244 6390

on track drilling
23795 Dewdney truck Rd
MAPLE RIDGE, BC V4R 1W1

July 31, 2018

Person/Business : ON TRACK DRILLING INC.
Account number : 685596

This letter provides clearance information for the purposes of Section 51 of the *Workers Compensation Act*.

We confirm that the above-referenced firm is active, in good standing, and has met WorkSafeBC's criteria for advance clearance. Accordingly, if the addressee on this letter is the prime contractor, the addressee will not be held liable for the amount of any assessment payable for work undertaken by the above-referenced firm to **October 01, 2018**.

This firm has had continuous coverage with us since February 28, 2002.

Employer Service Centre
Assessment Department

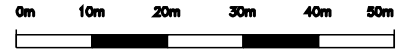
Clearance Reference # : C130386631
CLRAAA

For more information about Section 51 and clearance letters visit WorkSafeBC.com

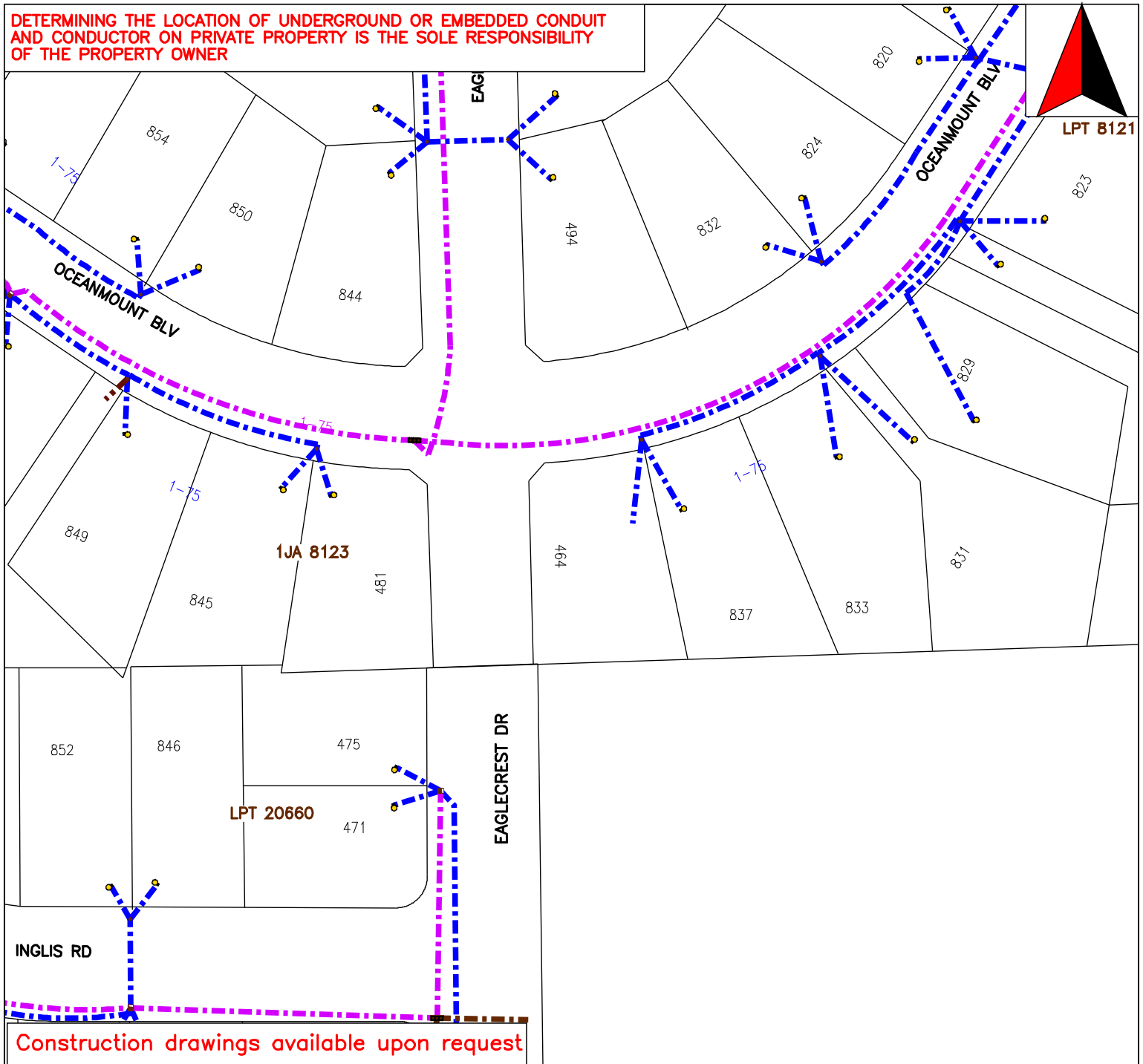
Please refer to your account number in your correspondence or when contacting the Assessment Department.

To alter this document constitutes fraud.

Street No. From: 464
Street No. To:
Street: EAGLECREST DR
City: GIBSONS



DETERMINING THE LOCATION OF UNDERGROUND OR EMBEDDED CONDUIT AND CONDUCTOR ON PRIVATE PROPERTY IS THE SOLE RESPONSIBILITY OF THE PROPERTY OWNER






THIS PRINT IS PROVIDED FOR GENERAL INFORMATION ONLY





BC Hydro does not accept any responsibility for errors or omissions. The information provided is the most accurate information we have available. Beware that underground electrical systems may exist that have not been record "AS CONSTRUCTED" yet.

The onus is on the operator to hand dig to locate the actual underground utility before any mechanized digging proceeds.

Legend

distribution underground [Gis]

-  Junction
-  Service Box
-  U/G Primary

-  U/G Primary
-  U/G Secondary
-  U/G Secondary
-  U/G Transformer

ABBREVIATIONS:
DP - Distribution Pressure
IP - Intermediate Pressure
TP - Transmission Pressure
PE - Polyethylene

DP GAS MAINS

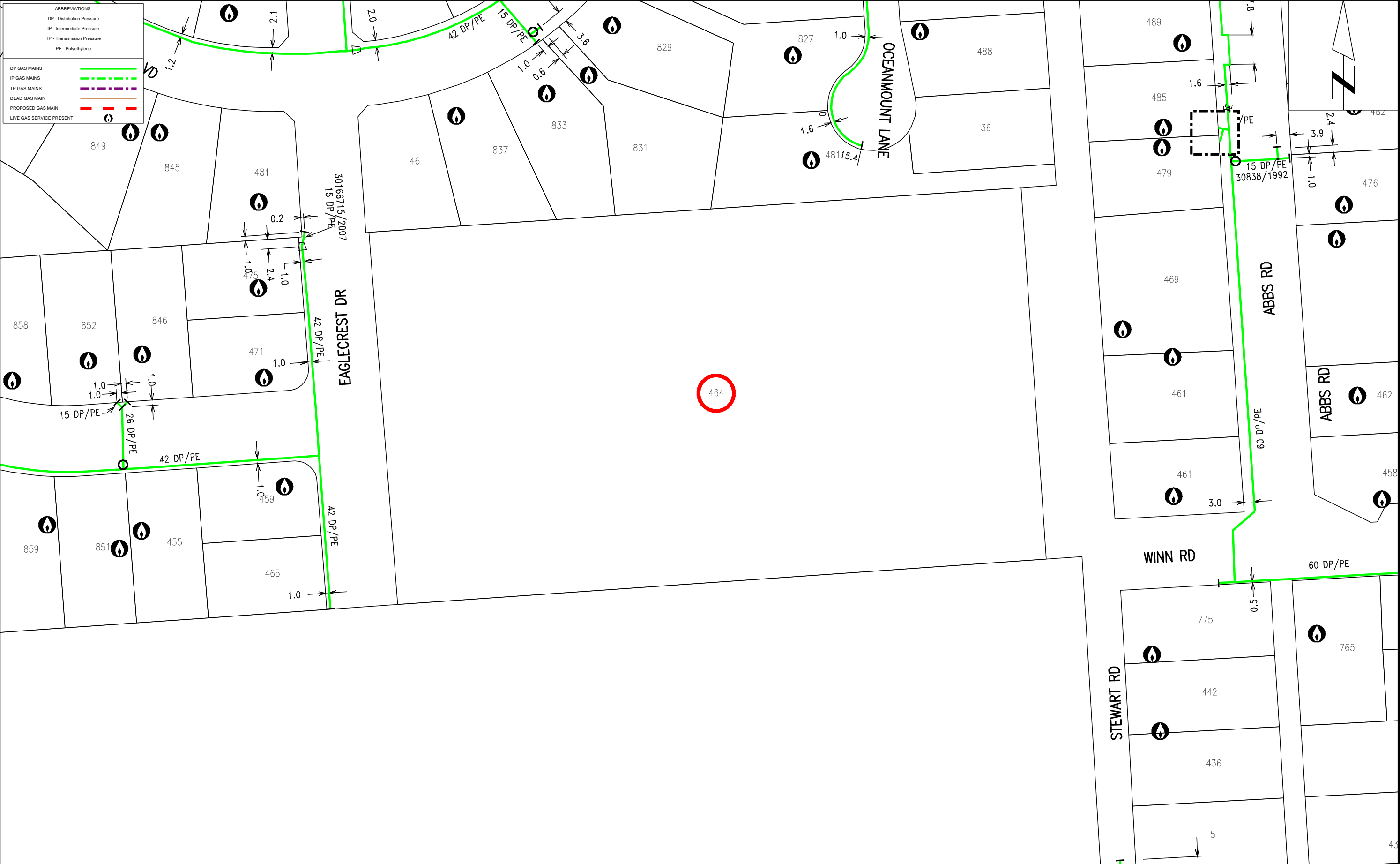
IP GAS MAINS

TP GAS MAINS

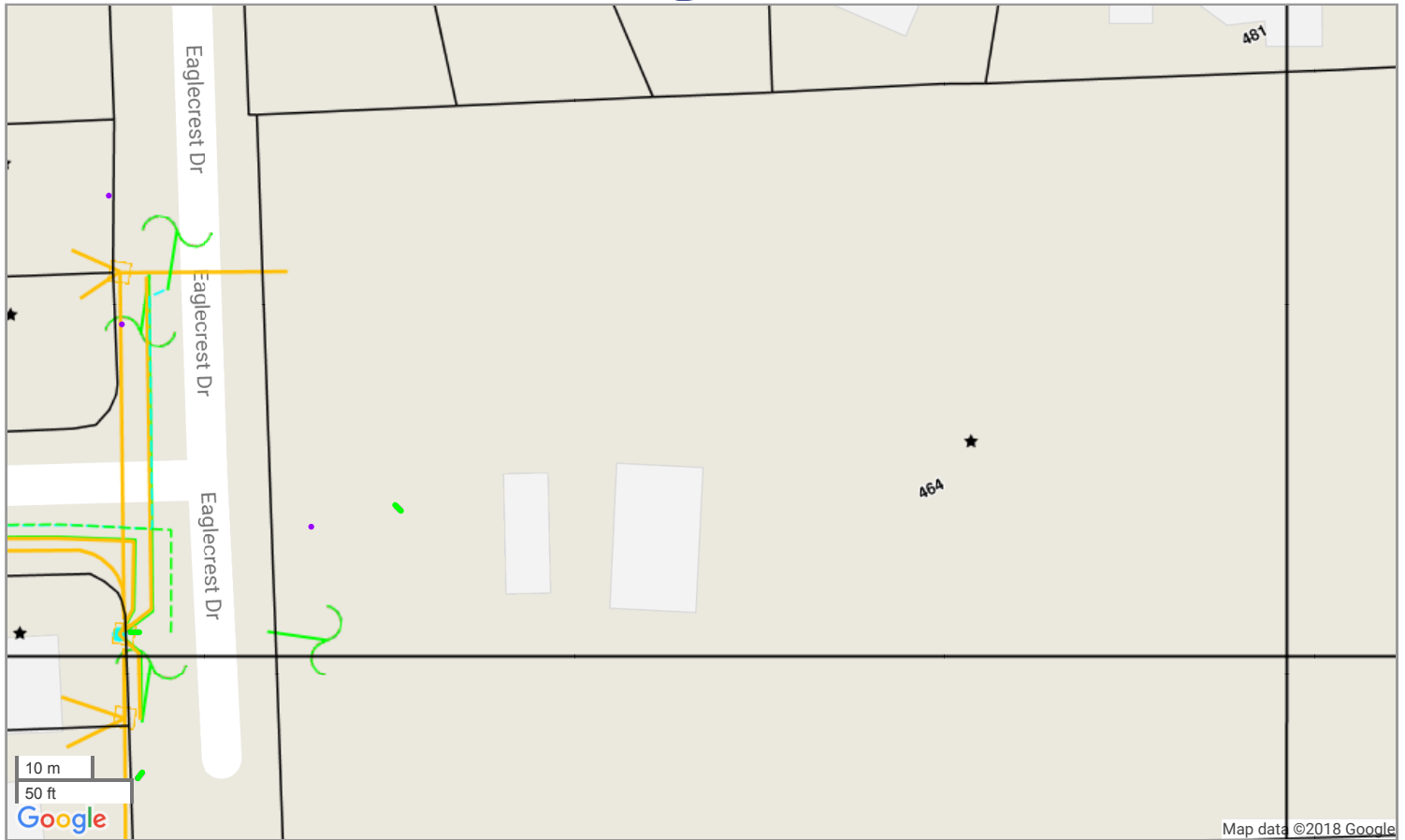
DEAD GAS MAIN

PROPOSED GAS MAIN

LIVE GAS SERVICE PRESENT



ATTENTION:
DO NOT RELY ON THIS INFORMATION ALONE!
You must hand dig to expose the line at several locations to determine its exact location and depth before using any mechanized equipment. All locations are approximate only. Gas lines built after the date shown, are not included in this information package. FortisBC will not accept responsibility for errors or omissions. Gas line depths are not available due to possible changes in grade. Record information provided is specific to location of original request from BC One Call. Measurements displayed in meter(s).



2018212789

THIS IS NOT AN AS-BUILT, THERE ARE NO MEASUREMENTS TO A FIXED OBJECT.
FOR REFERENCE ONLY, THIS DRAWING IS NOT TO BE USED IN PLACE OF A PHYSICAL
LOCATE OR LOCATE DRAWING.

EXCAVATOR IS RESPONSIBLE TO OBTAIN PRIVATE LOCATES AND ENSURE
UNDERGROUND FACILITIES ARE PROTECTED DURING EXCAVATION



2018212789

THIS IS NOT AN AS-BUILT, THERE ARE NO MEASUREMENTS TO A FIXED OBJECT.
FOR REFERENCE ONLY, THIS DRAWING IS NOT TO BE USED IN PLACE OF A PHYSICAL
LOCATE OR LOCATE DRAWING.

EXCAVATOR IS RESPONSIBLE TO OBTAIN PRIVATE LOCATES AND ENSURE
UNDERGROUND FACILITIES ARE PROTECTED DURING EXCAVATION

Flowing Artesian Wells

Water Stewardship Information Series



Table of Contents

What's the difference between a flowing artesian well and an artesian well?	1	Are there specific actions to avoid when flowing artesian conditions are present?	6
Why do wells flow?	1	How can flowing artesian well be constructed in bedrock aquifers?	7
Why is stopping or controlling artesian flow important?	2	How can flowing artesian well be constructed in unconsolidated aquifers?	7
How can flowing artesian conditions be determined before drilling?	2	What should be done if flowing artesian conditions are suddenly encountered?	7
What are the provincial regulatory requirements for controlling or stopping artesian flow?	2	What are the key factors in completing and equipping a flowing artesian well?	8
What does it mean to "control" artesian flow from a well?	3	How is the pressure or static water level for a flowing artesian well measured?	8
Will a flowing artesian well dry up if the flow is stopped or controlled?	3	How should flowing artesian wells be closed?	8
Are there any water quality concerns with flowing artesian wells?	3	How is a flowing artesian well disinfected?	9
Are there any other concerns with flowing artesian wells?	3	Further Information	9
What can be done with an existing flowing well?	4		
What if the flow is needed, for example, to increase the baseflow of a creek or stream?	4		
Are there some general guidelines for constructing a flowing artesian well?	4		
What are the key issues to be aware of when drilling a flowing artesian well?	5		

This booklet contains general information on flowing artesian wells for well drillers, groundwater consultants and well owners in British Columbia. The booklet provides general guidelines on flowing artesian wells and does not replace professional knowledge or experience.

What's the difference between a flowing artesian well and an artesian well?

An **artesian well** is a well that taps into a confined aquifer (see Figure 1). Under artesian pressure, water in the well rises above the top of the aquifer, but does not necessarily reach the land surface. A **flowing artesian well** is one that has been drilled into an aquifer where the pressure within the aquifer forces the groundwater to rise above the land surface naturally without using a pump. Flowing artesian wells can flow on an intermittent or continuous basis and originate from aquifers occurring in either unconsolidated materials such as sand and gravels or bedrock, at depths ranging from a few meters to several thousand meters. All flowing wells are artesian, but not all artesian wells are flowing wells.

Why do wells flow?

Flowing artesian wells can be found in two types of situations:

- the aquifer is confined by impermeable materials (i.e., confined beds where the static water level is above the top of the aquifer and land surface); or
- the aquifer is not confined, but the static water level is above the land surface.

Static water level is the level to which water will naturally rise in a well without pumping. For flowing artesian wells, the groundwater level or static water level can be expressed as a head (e.g., artesian head) and reported as a length (feet or meters above ground level) or pressure (pounds per square inch or psi).

Artesian conditions can be generated by geological and topographical controls (see Figure 1) or by topographical controls alone (Figure 2). In the former, water in an artesian well rises upward due to the pressure confined in the aquifer. Artesian wells are found in inclined confined aquifers sandwiched between layers of rock or overburden that are impervious or have low permeability. Water enters the exposed portion of the aquifer at a high elevation and percolates down through interconnected pore spaces. The water held in these spaces is under pressure (confining pressure or hydrostatic head) due to the high elevation from which it originally came. If a well is drilled from the land surface through the overlying impervious layer, the pressure inside the aquifer will cause the water to rise in the well. In areas where the pressure of the aquifer is great enough, the water rises above ground level resulting in a flowing artesian well.

Hydrostatic head (or confining pressure) is the vertical distance between the water level in the well and the top of the aquifer and is expressed in feet or meters of water or pressure (psi).

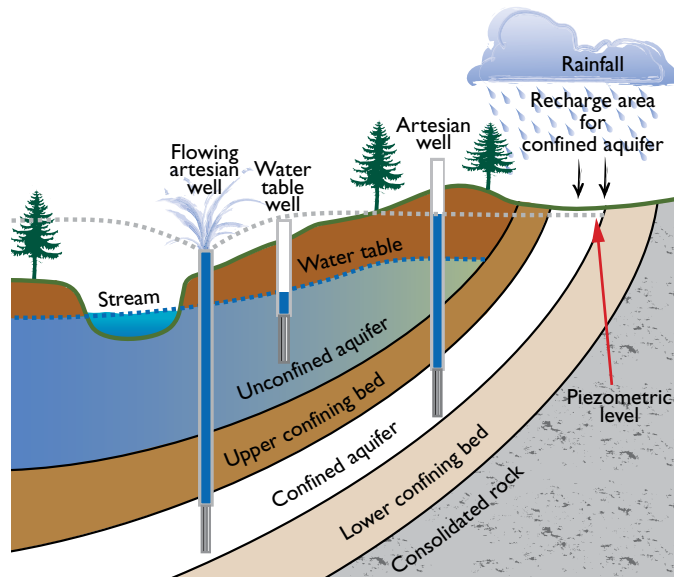


Figure 1. Geological and topographical controls affecting artesian and flowing artesian wells.

Topographical control situations can be found in unconfined aquifers where the well intake is deep enough to intercept a zone where the hydraulic head is higher than the land surface (see Figure 2). This situation typically occurs in groundwater discharge areas at lower elevations near rivers and lakes in valleys surrounded by steep slopes. The pressure of the groundwater typically increases with depth in the discharge areas where the slope of the water's

Hydraulic head is a measurement of the water level or total energy per unit weight above a datum such as sea level. It is commonly measured as water surface elevation in feet or meters.

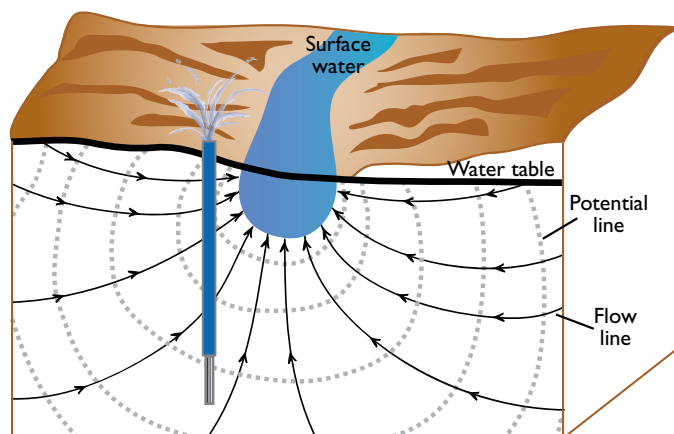


Figure 2. Topographically controlled flowing artesian well.

flow path and its pressure are controlled by the topography. As the groundwater moves along the flow path, it can migrate

deep below ground where it can lie beneath shallow non-artesian groundwater. When a well is drilled into a deeper zone of higher hydraulic head, the groundwater can move upwards inside the well casing to a level that is higher than the levels of the land surface, resulting in a flowing artesian well.

Why is stopping or controlling artesian flow important?

Flow from artesian wells should be controlled to prevent wasting groundwater. For instance, an uncontrolled artesian well flowing at 10 USgpm (55 m³/day) wastes 14,400 USgallons (55 m³) every day and 5.25 million USgallons (2.0 x 10⁴ m³) per year. An uncontrolled flow of 1 USgpm wastes enough water to supply four homes. Wasting water may lower the confining pressure in the aquifer so that the well no longer flows or flows at a reduced rate and affects the yield of neighbouring wells and springs.



Figure 3. Erosion caused by flowing artesian well.

When groundwater breaks out on the outside of the well casing, flooding, damage and/or subsidence and sinkhole formation can occur. Another reason to control flow is to prevent groundwater flowing from an aquifer under artesian pressure into an overlying aquifer(s). If the flowing well breakout is not promptly contained, silt, clay, gravel, sand, and drilling fluids can be carried along with the artesian groundwater to the ground surface and eventually reach surface water. The quality of the surface water and the habitat of aquatic organisms can be impacted.

Flowing artesian wells can also cause erosion (see Figure 3). Flowing water that accumulates into ponds can also contribute to mosquito problems.

How can flowing artesian conditions be determined before drilling?

Before a well is drilled, it is important for the person responsible for drilling the well (qualified well driller or qualified professional³) to do a pre-drilling assessment to determine the range of pressures and flows that might be found during drilling, i.e., whether flowing artesian conditions are likely to be encountered.

³ Qualified professionals who are registered with the Association of Professional Engineers and Geoscientists of British Columbia with competency in hydrogeology or geotechnical engineering.

The pre-drilling assessment should include gathering information about geological conditions, static water levels and any history of flowing artesian wells in the area. This information can be obtained from:

- reviewing available local well construction reports;
- reviewing hydrogeologic information (e.g., maps on the Water Resource Atlas http://www.env.gov.bc.ca/wsd/data_searches/wrbc/index.html showing flowing artesian well coverage (see Figure 4) or reports on Ecocat <http://www.env.gov.bc.ca/ecocat/>);
- consulting with the Ministry of Environment regional hydrogeologists; and
- consulting with well drillers and professional hydrogeologists or geotechnical engineers with knowledge of the local area.

If this information is not available, the person responsible for drilling the well should consider the proposed well depth in relation to relevant topographic and geologic information about the site (i.e., whether the proposed well is going to be deep in a valley-bottom location). Geophysical logs or an electric survey can also be used to better understand subsurface conditions. When knowledge is limited, a precautionary approach should be taken and planning should assume that flowing artesian conditions will be present.

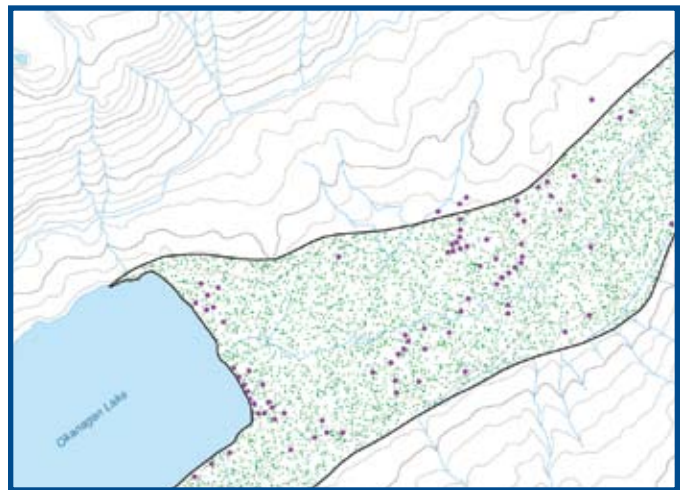


Figure 4. Map from the BC Water Resource Atlas showing provincial mapped and classified aquifers, contoured elevations and wells (purple dots) that were flowing artesian wells at the time drilling.

What are the provincial regulatory requirements for controlling or stopping artesian flow?

The provincial regulatory requirements for controlling flowing artesian wells are outlined in section 77 of the *Water Act*. If artesian conditions are encountered when constructing or supervising construction of a well, the qualified well driller

or qualified professional must ensure the artesian flow is or will be stopped or controlled and advise the well owner (and the land owner, if applicable) of the steps taken to do so. It is also good practice to advise of any potential hazards associated with uncontrolled flow not being controlled (e.g., erosion, flooding, subsidence) and any associated costs. Agreement on these issues, prior to drilling can help prevent or minimize misunderstandings. For example, some issues can be addressed in a contract. If the qualified well driller or qualified professional fails to stop or control the flow, it is the well owner's responsibility to hire another qualified professional or qualified well driller to ensure that the flow is stopped or controlled. If the ownership of the well is not known, the land owner is responsible to have this done. If the flow cannot be controlled, the person responsible for drilling the well should advise the Ministry of Environment's regional hydrogeologist and must comply with any direction given.

A flowing artesian well must have a securely attached cap to provide access to the well, prevent entry of vermin and contaminants, and to prevent flow escaping from the well.

What does it mean to “control” artesian flow from a well?

A flowing artesian well is considered “under control” when the entire flow is through the production casing to the wellhead and the flow can be stopped indefinitely without leaking on the surface of the ground and with no leakage into any other aquifer penetrated by the well.

Will a flowing artesian well dry up if the flow is stopped or controlled?

Controlling the flow from a flowing artesian well should not stop the flow or dry up the well if the well has been properly constructed. In fact, the opposite is true as waste of artesian water will often eventually cause a decrease in artesian pressure. Controlling the flow from a flowing artesian well prevents unnecessary loss of groundwater from the aquifer upon which other wells rely.

Are there any water quality concerns with flowing artesian wells?

In general, the water quality of flowing artesian wells is excellent. However, some artesian waters may be very poor quality and cause serious damage on the surface or contaminate an overlying aquifer. In general, water quality can be affected by the depth of the well, i.e., a deeper flowing artesian well may have poorer water quality than a shallower flowing well. Water from bedrock formations, such as deep sandstone formations, may contain concentrations of arsenic that could pose a health concern. Artesian wells with poor quality water should be permanently closed ([see page 8](#)).

Are there any other concerns with flowing artesian wells?

Most of the problems associated with flowing artesian wells result from improper discharge controls or improper well construction.

Casing corrosion ([see Figure 5](#)) and leakage can occur due to the constant flow of water, particularly if the water is corrosive



Figure 5. Corroded well casing.

or contains fine sand. Where artesian water is known to be corrosive, a smaller diameter flow pipe may be installed in the well. The pipe may be made of corrosion-resistant material or may be periodically replaced when it becomes corroded. Where the casing has been damaged, a slightly smaller diameter casing can be installed inside the old casing using packers if there is an existing surface seal and sealed in place with a cement grout. It is recommended to have the flowing artesian well checked periodically by a qualified well driller to verify the integrity of the well casing and to inspect the well screen, as the well can be difficult to repair once the casing has been corroded or breached. Thin-wall casing should not be used in flowing artesian wells.

Failure of the casing/surface seal during construction or decades after well completion can be costly and may result in the eruption of large volumes of silt, sand, clay or gravel, causing unstable conditions and potential flooding, damage to nearby structures through erosion and subsidence and harm to the habitat of aquatic organisms.

Well screens for flowing artesian wells can yield water with sand or become plugged with sand if the well is not properly developed. This is an issue when a flowing artesian well in a

fine-grained aquifer is shut off and the sand settles and clogs the area in and around the bottom of the casing. The screen size should be coarse enough to prevent pressure build-up in the aquifer and the well should be properly developed. Perforated casings for flowing artesian wells are not recommended. In some areas an unpleasant rotten egg smell (hydrogen sulphide gas) may be present and by reducing or stopping the artesian flow the smell can be brought under control.

What can be done with an existing flowing well?

Trying to stop or control the flow from older flowing wells may result in an uncontrolled discharge of water outside the well casing or at a distance from the well due to the lack of an adequate seal, a defective surface seal or corroded casings. If water does not appear to be flowing outside of the outer casing, then it may be advisable to leave the well alone and not restrict the flow. However, if water appears to be flowing outside the casing and/or the well is causing property or environmental damage, then the well should likely be closed. Alternatively, it may be possible to lower the water levels using a pump but care must be taken to keep the water flowing from the well relatively continuously to avoid additional uncontrolled discharge from occurring.

There are numerous special measures that may be applicable to controlling the flow of an existing flowing artesian well such as using well packers or a bridge to restrict the flow in the confining layer, adding polymers or plasticizers to keep the grout together during placement, using barite to reduce the confining pressure of the water, etc.

Any alteration to an existing flowing well to control the flow needs to be done in compliance with the *Water Act* and Ground Water Protection Regulation and any directions of a Ministry of Environment hydrogeologist. A qualified well driller or qualified professional must be hired. Before any work is done, the well owner should be made aware of the costs and complexities of the work involved with controlling the flowing artesian well, as well as the chances of successfully controlling the flow.

What if the flow is needed, for example, to increase the baseflow of a creek or stream?

In some instances, artesian flow is used to maintain water levels in ponds used for irrigation, fire protection, fish rearing, recreation or wetland enhancement. For existing wells, flow is permissible as long as property is not damaged and streams or aquatic habitats are not negatively impacted. If damage does or may occur, contact the local Ministry of Environment office ([see back cover of this booklet](#)).

Are there some general guidelines for constructing a flowing artesian well?

In constructing a well under flowing artesian conditions the potential pressure and flow and the permeability of the formation need to be taken into consideration. A pre-drilling assessment of local conditions may provide this information. If these conditions are known, the following provides general guidance for the design and construction of the well. If this information is not known the well should be designed conservatively for worse case conditions. Flowing artesian wells should not be constructed if the formation conditions are not favourable, i.e., in shallower situations where there is no suitable formation to seal into.

Green Zone (<5 psi)

If the pressure is or will be less than 5 psi (pounds per square inch), flow can usually be controlled by adding additional casing, except where permeability of the formation is extremely high, e.g., medium to coarse gravel. To determine the artesian head use the following conversion factors: 2.31 feet equals 1 psi, and one foot equals 0.3048 meters. For example, for a flowing well with 5 psi, there will be 11.6 ft or 3.5 meters of artesian head, therefore the casing would need to be extended more than 3.5 meters above the ground surface to contain all the artesian head. In general, a 30 per cent bentonite grout can be used for flowing well construction or repair.

Artesian head is the hydraulic pressure created within the confined aquifer that drives the water upward in a well to the piezometric level. The distance from the ground surface to the piezometric level, converted into equivalent pressure (expressed as pounds per square inch, or PSI), is the artesian head.

Yellow Zone (5 to 10 psi)

If the pressure is or will be between 5 and 10 psi, extending the well casing may reduce flow, but extreme care must be taken in highly permeable formations that produce significant volumes of water. Flows of 20 USgpm can potentially occur in this zone and the upward annular velocity resulting from this flow is high enough to begin separating grout mixtures as they are being pumped down. When the pressure is high and the formation highly permeable, it is recommended that an outer surface casing be installed before the permanent casing. The outer casing should end in the confining layer and should not penetrate the underlying artesian aquifer. Cement-type grout should be used.

Red Zone (>10 psi)

If the pressure is or will be greater than 10 psi, static head control or extending the well casing is not usually possible, especially in highly permeable, high-yielding formations. In this category the flow is great enough to make the grout placement very difficult. An outer casing or multiple casings should be installed before the production casing and set to

the confining layer so the production casing can be cemented within the outer casing. Cement or cement plus barite (or other weighting additives) should be used as grouting materials.

What are the key issues to be aware of when drilling a flowing artesian well?

Flowing artesian wells under high pressure and with high flow rates (yellow and red zones) are challenging to construct. Flowing wells that are drilled deep (≥ 200 feet or ≥ 60 meters) in unconsolidated deposits or drilled into bedrock are less prone to flow problems and are generally easier to deal with. In bedrock environments (see page 7 for more information on bedrock wells), the competent rock allows for easier installation of the seal (i.e., no casing to wash out or concerns about an eroded annulus).

Drilling a well into a confined aquifer disturbs the overlying geologic confining layer and provides a potential pathway for the upward movement of the pressurized artesian water. Well construction must include restoring any damage to the confining layer. In general, the closer the top of the artesian formation is to the ground surface and the higher the pressure, the more difficult it is to control the flow.

In certain conditions (e.g., soft clay/silt formations), the formation will squeeze back in and set up around the well casing over a period of time. If this condition is likely to occur, it is advisable to let the well flow for a week or two to give the formation a chance to settle in before stopping or controlling the flow. This will result in a seal around the casing at deeper depths than the surface seal.

It is good practice for the qualified well driller to observe the condition of the flowing artesian well head for one or two weeks after construction and check for leakages outside the surface casing or between casings.

Materials and Equipment

One of the key factors to successfully controlling the flow is being prepared with the right tools and materials at the job site. Suggested materials and equipment include:

- drilling mud and additives of sufficient weight to deal with the pressures in the aquifer,
- surface and production casing appropriate to the water quality and geological conditions,
- grouting and sealing materials appropriate to the artesian pressure and anticipated flow,
- tremmie pipes,
- pumps suitable for delivering the grouting and sealing materials,
- well screens with adequate transmitting capacity,
- valves,
- inflatable packers,
- surge block, and
- shale traps.

Drilling Muds

To determine the extra weight of drilling mud needed to counteract the pressures of the artesian aquifer during rotary drilling, the estimated artesian head and the depth to the top of the aquifer is needed. The following formula can be used to estimate the additional weight of drilling mud needed to control the flow during the drilling process:

$$\text{Additional mud weight} = \left(\frac{8.34 \text{ lbs/USgal} \times \text{height of water above ground level (ft)}}{\text{Depth to top of aquifer (ft)}} \right) + 0.4 \text{ lbs/USgal}$$

Where:

One USgallon of water weighs 8.34 pounds

0.4 lbs/USgallon is a safety factor

Example

If the depth to the top of the aquifer is 75 feet and the height of water above ground is estimated to be 10 feet, the additional weight of drilling mud needed would be $(8.34 \times 10/75) + 0.4 = 1.5 \text{ lbs/USgal}$.

Properly mixed, fresh drilling mud will normally weigh about 9 pounds per US gallon. Drilling mud can be made heavier by adding drilling clay, drilling gel and special solids such as barite. However, some drilling gels are treated with polymers to build viscosity and become difficult to pump before their weight significantly increases. Therefore, some drilling gels have limited ability for control of flows. Mud weights of up to 15 pounds per gallon can be achieved using weighting materials such as powdered barite.

Well Casings

Generally, in areas where flowing artesian conditions are known or suspected, at least one outer surface casing should be installed before installing the permanent/production casing or liner to allow for better control. It is not advisable to pull the surface casing within 20 feet (6 meters) of ground surface. Doing so may disturb the seals and cause water to flow around the surface casing as it is pulled, especially if bentonite is used. There should be at least a 4-inch (10 cm) gap or annulus between the outer surface casing and the production casing to allow for the insertion of a tremmie pipe to pump adequate grout volumes. For example, if a 6-inch production casing is needed, a 14-inch outer surface casing would have to be installed to provide a 4-inch annulus.

In areas where the pressure is > 5 psi and the formation is highly permeable, a 4 to 6-inch (10 to 15 cm) annulus between the surface and permanent casing is recommended. Ensuring there is an adequate annulus is especially important where formations are highly permeable and high-density grout mixtures are required to adequately control the artesian flow.

Grouting Mixtures

Use of appropriate grouting material is key to constructing a flowing artesian well. Table 1 is useful for finding the hydrostatic




head pressure (in psi) and for understanding the relationship between drilling fluid or grout density and their ability to successfully control the flow during drilling, plugging, or repair. Table 1 shows that heavy grouts, such as neat cement/bentonite slurry or cement slurry with additives, have a distinct advantage for flowing well work. Mixing neat cement with bentonite is recommended to avoid cracks from occurring.

It is important to allow for sufficient time for the cement or cement grout mixture to set before proceeding with drilling. Use of the appropriate drilling method to minimize impacting the integrity of the seal is also important. In addition, the flowing artesian well should be gradually sealed or shut-in to prevent rupturing the seal(s).

TABLE 1 TOTAL PRESSURE ABOVE TOP OF CONFINED AQUIFER (HYDROSTATIC PRESSURE) FOR FLOWING ARTESIAN WELLS						
Depth to Top of Flowing Aquifer (feet)	Artesian Head Above Ground Surface (feet)					
	5	10	15	20	25	30
10	6.5	8.7	10.8	13.0	15.2	17.3
20	10.8	13.0	15.2	17.3	19.5	21.7
30	15.2	17.3	19.5	21.7	23.8	26.0
40	19.5	21.6	23.8	26.0	28.1	30.3
50	23.8	26.0	28.1	30.3	32.5	34.6
75	34.6	36.8	39.0	41.1	43.3	45.5
100	45.5	47.6	50.0	52.0	54.1	56.3
125	56.3	58.4	60.6	62.8	65.0	67.1
150	67.1	69.3	71.4	73.6	75.8	78.0
175	78.0	80.1	82.3	84.4	86.6	88.7
200	88.7	91.0	93.1	95.2	97.4	99.6
225	99.6	101.7	104.0	106.0	108.2	110.4
250	110.4	112.5	115.7	117.0	119.0	121.2

Adapted from the Michigan Department of Environmental Quality, Water Bureau, Lansing, Michigan

Material	Weight	Hydrostatic Pressure
Barite Slurry:	18 - 22 lb/USgal	.96 - 1.1 psi/ft
Neat Cement and Bentonite @ 6 gal water/sack:	15.0 lb/USgal	.78 psi/ft
Bentonite Slurry Grout:	10.4 lb/USgal	.54 psi/ft
Bentonite Slurry Grout:	9.5 lb/USgal	.49 psi/ft

GROUTING MATERIAL SUITABILITY	
Heavy Enough To Overcome Hydrostatic Pressure	Not Heavy Enough To Overcome Hydrostatic Pressure
 Neat Cement @ 15 lb/USgal	All Bentonite Grouts
 Neat Cement @ 15 lb/USgal or Bentonite Grout @ 10.4 lb/USgal	Bentonite Grouts lighter than 10.4 lb/USgal
 All standard grouts have enough weight to overcome hydrostatic pressure of the flow.	

The values in Table 1 correspond to the downhole head pressure (in psi) for different scenarios, e.g., if the depth to the top of the aquifer was 10 feet and the artesian head was 5 feet, the downhole head pressure will be 15 feet or 6.5 psi. To overcome the flow, the downhole grout pressure must be greater than the downhole head pressure.

The following example illustrates how Table 1 can be used to select drilling fluids or grout that are heavy enough to control the flow during drilling.

Example of how to use Table 1

Q. *The top of an artesian aquifer is found at 50 feet and wells in the area have about 15 feet of artesian head. What minimum weight drilling fluid would be needed to overcome the hydrostatic pressure during drilling?*

A. The following steps are used to solve the problem:

Step A: To determine the downhole hydrostatic head pressure look at **Table 1** and find the cell corresponding to depth of top of aquifer (50 ft) and artesian head (15 ft) which is 28.1 psi. This pressure represents the total head above the top of the confined aquifer (e.g., 15 + 50 = 65 ft or 28.1 psi).

Step B: Divide the downhole hydrostatic pressure (28.1 psi) by the depth to the top of the aquifer (50 ft) to determine the downhole grout pressure needed to equalize the flow (28.1 psi/50 ft = 0.56 psi/ft).

Step C: To determine the grout weight divide the downward pressure of the grout (0.56 psi/ft) by 0.052 (a factor to convert lb/USgal to psi/ft of depth). The minimum grout weight needed to control the flow is 10.8 lb/USgal.

Are there specific actions to avoid when flowing artesian conditions are present?

When a large volume, high pressure flow breaks out, the immediate situation can be serious and there is usually a concern to quickly move the drilling rig away from the borehole. Hastily made decisions can get in the way of successful future corrective actions. As up-flowing artesian water typically will erode fine sediments around a solid object that has been placed loosely below ground, the following actions should be avoided:

- dumping field stone or gravel into the annulus around the well casing as this can prevent the installation of grout pipes or a larger casing into the borehole and can collapse PVC well casing;
- pouring ready-mix concrete or bentonite chips into the annulus as it is likely that the concrete or bentonite will solidify above the depth where the flow is originating and

result in a plug that causes the flow to wash out around its perimeter; or

- jamming unopened bags of cement, bentonite chips, lumber, cardboard or other debris into the washed out annulus as these materials are ineffective and complicate further corrective action.

How can flowing artesian wells be constructed in bedrock aquifers?

When constructing an artesian well that is likely to flow in a **bedrock aquifer**, the final or outer well casing should be sealed at least 10 feet (0.3 meters) into competent bedrock. [Figure 6](#) shows one possible method of completing a flowing artesian well in bedrock. Construction techniques and choice of sealant materials need to be determined by the qualified well driller based on site specific conditions, e.g., pressure and flow.

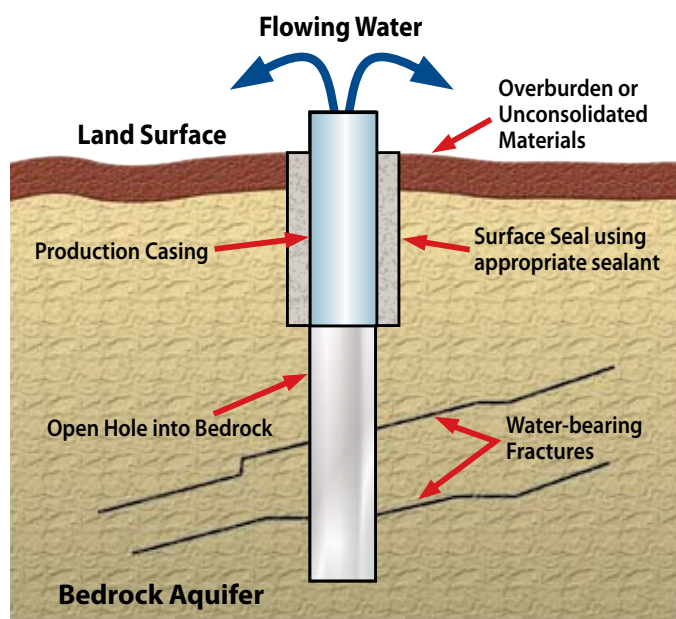


Figure 6. One possible method of completing a flowing artesian well in a bedrock aquifer.

How can flowing artesian wells be constructed in unconsolidated aquifers?

For **confined, unconsolidated aquifers** where flowing artesian conditions are likely, a cased oversized hole should be drilled into the confining layer, to allow a cement, or high solids bentonite seal to be placed between the final production casing and the outer casing (see [Figure 7](#)). This can be very complicated and expensive if the pre-drilling assessment indicates the confining layers are more than 100 ft (30 metres) deep. The size of the hole or casings and the depth of the seal must be determined on a site-by-site basis since choices are influenced by local geology and the specific artesian conditions encountered. A careful, conservative approach is recommended.



Figure 7. Bentonite cement grout seal between casings.

When constructing a well into a confined, unconsolidated flowing artesian aquifer, the appropriate sealant material between the outermost well casing and the confining layer must be of a sufficient depth and thickness to contain the flow.

Artesian conditions in **unconfined, unconsolidated aquifers** require special construction techniques such as using heavier drilling mud to counteract the pressure of the aquifer and a temporary surface casing to prevent hole collapse.

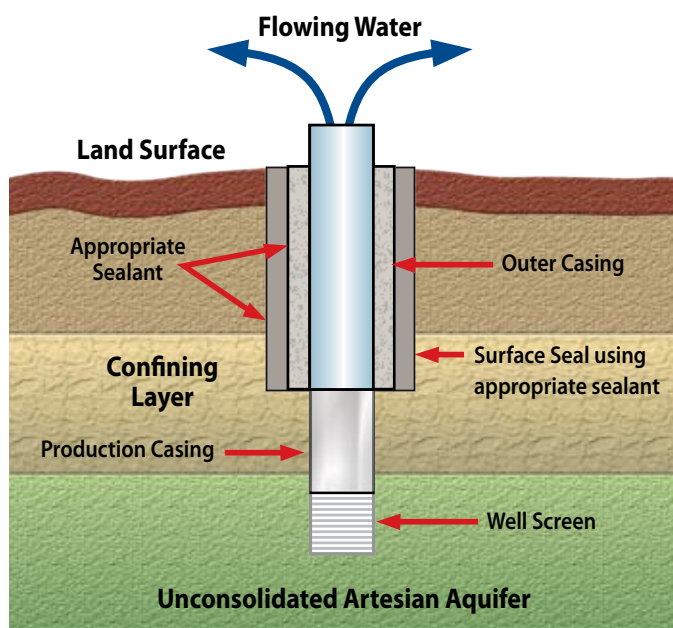


Figure 8. One possible method of completing a flowing artesian well in unconsolidated materials, e.g., sand and gravels.

What should be done if flowing artesian conditions are suddenly encountered?

When unexpected flowing artesian conditions are encountered (i.e., instant flow occurs), a qualified professional, or qualified well driller, should take control of the site and equipment should not be removed from the site until the artesian flow is under control. Contact the owner of the well and the land owner immediately

to report the situation and provide plans to control the flow (see below). Steps to take include:

- control the flow,
- secure the casing or borehole, and
- protect the drill rig.

The flow may be brought under control by:

- increasing the weight of the drilling mud,
- using plugs,
- using a surge-blocking to restrict flow, or
- installing a drillable packer.

The drill pipes can be left in place in cases where the uncontrolled flow occurs in an uncased drill hole, to indicate the exact location of the hole.

If the flowing artesian well is discharging water into a wetland or surface water body, contact the local Ministry of Environment office.

It is important for the well owner (and land owner if applicable) to develop a clear understanding, potentially in the form of a contract, with the drilling contractor on how the well will be repaired and/or the flow stopped or controlled before any work on the well commences to avoid or minimize potential misunderstandings when artesian flow is encountered.

What are the key factors in completing and equipping a flowing artesian well?

Flowing artesian wells, when properly constructed, should be equipped with a device to completely stop or control the artesian flow from the well (see Figure 9). After flow is stopped, there should be no leakage up the annulus between the outermost casing and the borehole. If water does escape, the annulus should be sealed.



Figure 9. Completed high pressure flowing artesian well.

Flowing artesian wells, like all wells, need to be vented. Well caps should be equipped with a two-way vent that allows the well to inhale and exhale air as the water level changes during pumping cycles. The vent will seal the well when the pump is not in use.

Determine the shut-in pressure (see below) and record the measurement on the well construction report. The wellhead should also be designed and equipped to prevent any backflow into the well.

Where freezing conditions may occur, the wellhead of the new flowing artesian well should be covered, insulated and heated, where necessary, to prevent damage of the flow control device leading to an uncontrolled flow situation.

How is the pressure or static water level for a flowing artesian well measured?

It is important to determine and record the hydrostatic pressure of the flowing artesian well for future pre-drilling assessments. There are several ways to measure the hydrostatic pressure or static water level of a flowing artesian well:

1. Extend the well casing, or a smaller diameter pipe through a well seal on the top of the casing, high enough above the ground surface until water no longer flows out the top (without pumping). The water level in the casing extension can then be measured using a water-level sounder. The distance from the piezometric water level in the casing to the ground surface is the artesian head of the aquifer – this can be converted to pressure.

2.31 feet equals 1 psi or
0.433 psi equals 1 foot

Example

A static water level of 30 feet is converted to pressure by dividing 30 feet by 2.31 feet/psi = 13 psi.

2. A pressure gauge installed on a well seal at the top of the casing will provide the pressure reading which can be multiplied by 2.31 to find the artesian head at the gauge elevation.

How should flowing artesian wells be closed?

A qualified well driller and/or qualified professional should be hired to close a flowing artesian well and ensure that the well is closed in such a manner that there is no leakage at the surface of the ground (see Figure 10). The driller must be prepared to handle the flow from the well and the discharge of any plugging materials immediately on removal of the flow control device(s). The work site can be dangerous if the flow is not properly diverted. Closing a flowing artesian well is simplified if the flow can be overcome by extending the well casing above the artesian head. Alternatively, insert an inflatable packer or expandable rubber plug at the bottom of the casing. Physically stopping the flow may make things worse, however, which is why the rapid loading of drilling gel is often a better approach.

Another effective approach is lowering the water level by pumping from adjacent wells. A leaking annulus should be sealed (if possible) before proceeding with grouting the production casing.

Pump a high density grout such as neat cement or concrete grout with bentonite through a PVC pipe or drill rod which is lowered to the bottom of the well. The cement mixture is pumped until it reaches the land surface. Pressure grouting with a packer may be required. It may also be good to pull or perforate some of the casing to allow the grout to flow from the casing into the annulus, although this is not critical if the casing is already perforated or corroded.

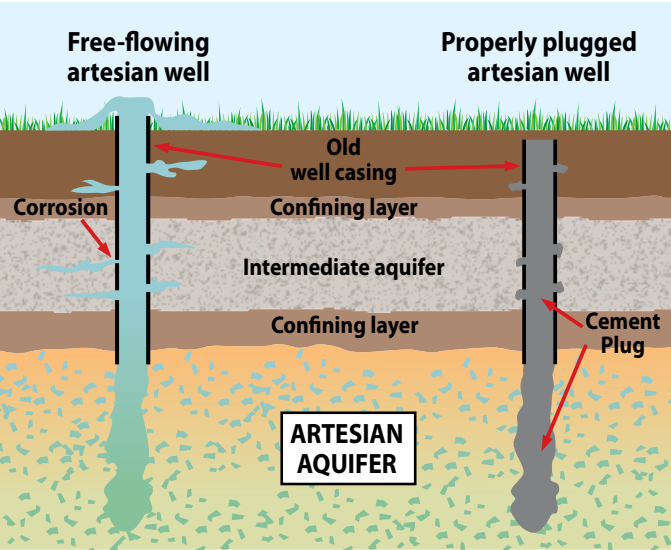


Figure 10. Example of a properly closed flowing artesian well.

How is a flowing artesian well disinfected?

Because of the protected nature of the confined artesian aquifer, flowing wells are generally less prone to bacterial contamination. Furthermore, the positive artesian pressure can minimize entry of surface contaminants into the well. Contamination introduced during the drilling process may be flushed out by the continuous discharge of water.

To disinfect a flowing well using chlorine, a temporary casing extension above the piezometric level or a tight well cap or seal can stop the flow and increase the chlorine contact time. A chlorine solution can also be pumped into the well via the secure well cap and hose connections. Once the casing extension or cap is removed, the well discharge will flush residual chlorine and inactivated bacteria from the well.

If the chlorinated water has a potential to harm the environment (e.g., fish), use an effective neutralizing agent, such as Vitamin C, to inactivate the chlorine. A solution of at least 1 per cent (by weight) of ascorbic acid is the most cost-effective form of Vitamin C. Added to the sump or a stream of chlorinated water, reaction time is nearly instantaneous.

Further Information

A registry of qualified well drillers can be found at: http://www.env.gov.bc.ca/wsd/plan_protect_sustain/groundwater/wells/applications/well_drillers_reg.pdf.

A listing of groundwater consultants (qualified professionals) can be found at: http://www.env.gov.bc.ca/wsd/plan_protect_sustain/groundwater/library/consultants.html.

Michigan Department of Environmental Quality, 2005. Flowing well handbook: http://www.michigan.gov/documents/deq/deq-wb-dwehs-wcu-flowwellhandbook_221323_7.pdf.

For further information on whether approvals are needed for discharging flowing artesian well water to surface water bodies, contact the local Ministry of Environment office:

Vancouver Island Region	Nanaimo	250-751-3100
Lower Mainland Region	Surrey	604-582-5200
Thompson and Cariboo Regions	Kamloops	250-371-6200
Kootenay and Okanagan Regions	Nelson	250-354-6333
	Penticton	250-490-8200
Omineca Peace and Skeena Regions	Prince George	250-565-6135



Photos by Jim Fyfe, David Martin, Mike Simpson, Peter Epp & Thierry Carriou.

ISBN 978-0-7726-7034-2

**Foundations,
Excavation &
Shoring
Specialists**

Braun Geotechnical
102 19049 95A St
Surrey, BC V4N 4P3
Tel: 604-513-4190
Fax: 604-513-4195
info@braungeo.com

www.braungeo.com



October 24, 2018

Reference: 18-7707

Via email: kthomas@gibsons.ca

Town of Gibsons
474 South Fletcher Road
Box 340
Gibsons, BC, V0N 1V0

Attn: Katie Thomas, Planner1

Re: ESC Geotechnical Field Reviews – DPA9
Proposed Residential Development
464 Eaglecrest Drive, Gibsons, BC

1.0 INTRODUCTION

As requested, Braun Geotechnical Ltd. has carried out this geotechnical letter in support of a Stormwater management DPA9 permit application with Town of Gibsons for 464 Eaglecrest Drive, Gibsons, BC.

2.0 EROSION SEDIEMENT CONTROL PLAN REVIEW

Braun Geotechnical have reviewed the Aplin Martin Erosion and Sediment Control Plan drawings for 464 Eaglecrest Drive, Project No. 16-276 and dated June 2018.

The proposed temporary works to create an ESC pond are suitable with respect to geotechnical considerations.

3.0 TEMPORARY WORKS FIELD REVIEWS

Geotechnical construction field reviews are required by the Geotechnical Engineer of Record and would be completed by Braun Geotechnical at time of construction. Geotechnical field reviews would include but not be limited to excavation and placement of geomembrane/drain rock for ESC pond.

4.0 CLOSURE

We hope the above meets with your requirements. Should any questions arise, please do not hesitate to contact the undersigned.

Yours truly,

Braun Geotechnical Ltd.

A handwritten signature in blue ink, appearing to read 'Hugh MacMurray'.

Hugh MacMurray, EIT
Geotechnical Engineer

Braun Geotechnical Ltd.

A handwritten signature in blue ink, appearing to read 'Stuart Hrysiw', is placed over a circular green professional seal. The seal contains the text 'PROFESSIONAL ENGINEER', 'S.V. #30855', and 'B.C. GEOTECHNICAL ENGINEERING'.

Stuart Hrysiw, P.Eng.
Geotechnical Engineer

